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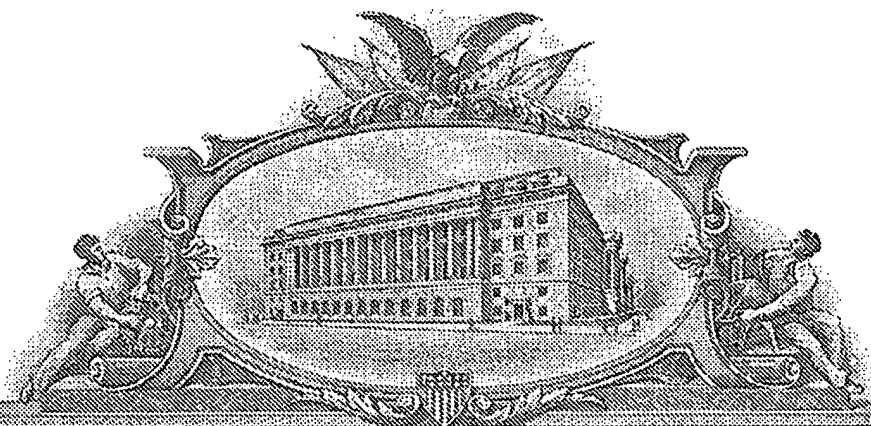
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**APPLICATION NUMBER: 60/536,535**

**FILING DATE: January 15, 2004**

**RELATED PCT APPLICATION NUMBER: PCT/US05/01233**



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16898 U.S. PTO

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This is a request for filing a PROVISIONAL APPLICATION FOR PATENT under 37 CFR 1.53(c).

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Additional inventors are being named on the _____ separately numbered sheets attached hereto					
TITLE OF THE INVENTION (500 characters max)					
INTEGRAL BRITTLINES TEST DEVICE AND METHOD					
Direct all correspondence to: CORRESPONDENCE ADDRESS					
<input type="checkbox"/> Customer Number: _____					
OR					
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ENCLOSED APPLICATION PARTS (check all that apply)					
<input checked="" type="checkbox"/> Specification Number of Pages 5					
<input checked="" type="checkbox"/> Drawing(s) Number of Sheets 2					
<input type="checkbox"/> Application Date Sheet. See 37 CFR 1.76					
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[Page 1 of 2]

Respectfully submitted,

Date Jan. 8, 2003

SIGNATURE \_\_\_\_\_

REGISTRATION NO. \_\_\_\_\_

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(If appropriate)

Docket Number: 1068/38

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**[Page 2 of 2]**

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Dear Sirs,

Re: New US Provisional Patent Application  
HIRSHBERG et al.  
**INTEGRAL BRITTLINES TEST DEVICE AND METHOD**

Enclosed please find attached a new provisional patent application.

Enclosed documentation includes:

- 1) Specification – 5 pages (2 copies)
- 2) Drawings – 2 sheets (2 copies)
- 3) Provisional Application for Patent Cover Sheet (form PTO/SB/16), duly signed by first named inventor.
- 4) Credit Card Payment Form

Please direct all correspondence in this case to the first named inventor:

Arnon HIRSHBERG  
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Very truly yours,

  
Doron Sieradzki

## **INTEGRAL BRITTLENESS TEST DEVICE AND METHOD**

The present invention relates to an integral brittleness test device and method for measuring the strength of brittle, deformable microstructures.

### **Problem Solved by the Invention and its environment:**

The present invention relates to the reliability of brittle, deformable structures that are prevalent in Micro-Electro-Mechanical-Systems (MEMS). Main aspects of the present invention address the following considerations: 1) measuring the ultimate strength of the structure in question (i.e.,  $\sigma_{uts}$ ). 2) conducting said measurement without the necessity of measuring forces or displacements. 3) Conducting said measurement without the necessity of packaging or special handling of the test device (i.e., in microsystems the test can be performed at the "wafer level" without requiring dicing).

Characterization of the strength of deformable elements in MEMS is important for design, and for estimation of reliability. The strength of such elements depends on mechanical properties of the structural material and is strongly affected by the surface texture that is formed during the fabrication process.

### **Closest Known Related Technology:**

Current techniques for characterizing the strength of structural elements in MEMS devices require real-time measurement of displacements and measurement of the applied forces. In some devices (see Fig.1) a "Dog-bone" test structure is axially tensioned up to failure [1]. In these devices failure can occur anywhere along the specimen. In other devices a cantilevered beam is deflected up to failure (see Fig.2), which inevitably occurs at the clamped edge [2]. In both techniques, the maximal applied force is either directly measured, or is deduced from direct measurement of the deflection (and known elastic constants of the tested material). Also, in both techniques the exact location of the failure provides no additional information on the mechanical properties of the structural material.

### **Novelty**

The new test device and method require no measurement of the applied forces or of the resulting deformation. They only require a measurement of the length of the remaining ligament. Due to the simplicity involved in the present invention, the integral test device can be used at the wafer-level (i.e., before dicing) and may be used to calibrate and examine the repeatability of the micromachining process.

### **Advantages of the Invention:**

The present invention has several advantages over the conventional solutions to the problems described above.

- 1) It only requires a measurement of the length of the remaining ligament, In contrast to previous techniques that require dedicated equipment to measure forces or displacements.
- 2) Due to the simplicity of its operation, this device can be used at the wafer-level (i.e., before dicing), In contrast to previous techniques that require delicate handling or expensive packaging process.
- 3) May be used to calibrate and examine the repeatability of the micromachining process.
- 4) May be used to characterize the uniformity in serial processing of wafers.

### **Full Description of the Invention:**

Cantilever beams are deformed up to failure by application of an unmeasured force. The ultimate tensile strength of the beams is directly deduced from the length of the remaining intact ligament of the broken beam.

The maximal tensile stress in a bent beam is equal to the product of the beam curvature, half of the beam width ( $h$  in Fig 3a), and the effective elastic modulus. The elastic modulus of the silicon is known and the beam width is measured (for example by optical means). By knowing the exact curvature of the beam at the point of failure, the ultimate tensile strength may be deduced. The cantilever beam in the new test device is wrapped over a wall with prescribed curvature. (For example if the wall is designed such that its curvature is linearly proportional to the circumferential distance from the clamped edge of the beam (see Fig.3). Accordingly, when the beam fails (breaks), the length of the



remaining ligament of the beam is linearly proportional to the ultimate tensile strength.) Note that the prescribed curvature does not necessarily have to be linearly changing curvature, and in fact any prescribed curvature is suitable.

The wrapping of the beam over the curved wall is preferably performed by a micro-manipulator, and the length of the remaining ligament is preferably optically measured (see Fig.3b).

The new device (see Fig.3) may be fabricated from mono-crystalline Silicon with known mechanical properties. However, the beams in this device are preferably micromachined using DRIE - Deep Reactive Ion Etching and their strength depends on the texture of the surface created by this fabrication process.

Many devices are fabricated using this process and usually the process parameters are found by trial and error or by previous experience. This present device and method can shorten the tuning time required to stabilize the process by deducing a direct result for the maximum strength capabilities.

During production this present device and method can be used as a characteristic for the whole wafer, to decide if the wafer continues the process flow or is thrown away (as in "pass / fail" test).

The present invention may be incorporated in the fabrication of wafers by way of including the device in a wafer in order to facilitate in-situ tests.

## **CLAIMS**

1. A device for measuring the tensile strength of a brittle material, the device comprising:

a main body with an integral cantilever beam, the main body having a curved wall, the curved wall designed such that its curvature is known .

2. A method for measuring the tensile strength of a brittle material, the method comprising:

imposing a changeable curvature over a cantilever beam, up to failure (break) of the beam and by measuring the remaining ligament length, deducing the maximum tensile strength.

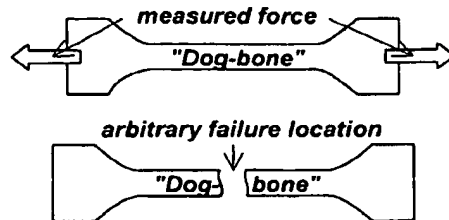


Figure 1: A "Dog-bone" tension test device. The applied force at failure must be measured. The location of failure provides no additional information.

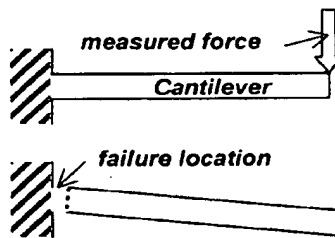


Figure 2: A cantilever test structure. The applied force must be measured. The failure always occurs at the clamped edge.

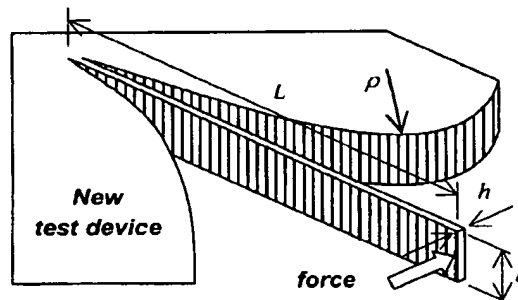


Figure 3a: A schematic description of the new test device. The curvature of the cylindrical wall increases linearly with distance from the clamped edge of the beam.

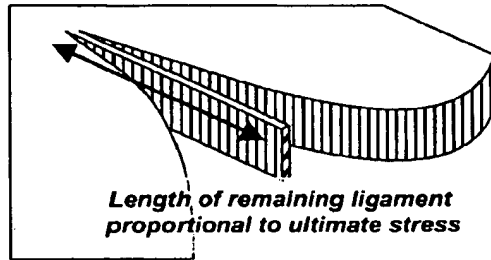


Figure 3b: The length of the remaining ligament after failure is linearly proportional to the ultimate strength of the structural material.